Overview of Fabrication

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Outline

- Building a Bridge Girder
 - How we do it know
 - Welding
 - Inspection
 - Efficient Sizing for Fabrication
 - How we want to do it in the future
 - Virtual Assembly



Modular Design Crane and Wrenches Required for Assembly No Post Tensioning Required





Typical Girder Proportions

• Transverse Stiffeners only as Required





Typical Girder Proportions 200 ft. Span

Span/Depth=25-30

 $D = 8 \text{ ft} \qquad \frac{S}{D} \le 25$

• $\frac{D}{t_w} \le 120$ $\frac{2D_c}{t_w} \le 137$

$$t_w = \frac{7}{8}$$
 in. $\frac{D}{t_w} = 110 \le 120$

• Compression Flange $-\frac{1}{4} > \frac{b_f}{D} > \frac{1}{6}$

$$b_f = 24$$
 in. $\frac{b_f}{D} \le 0.25$

$$-\frac{b_f}{2t_f} \le 12 \text{ and } < 9.2 \text{ for } 50 \text{ ksi}$$

$$t_f = 1.375$$
 in. $\frac{b_f}{2t_f} = 8.7$



Cross Sectional Limits AASHTO LRFD Specifications 6.10.2.2—Flange Proportions

Compression and tension flanges shall be proportioned such that:

$\frac{b_f}{2t_f} \le 12.0,$	Too slender, 9.2 for Grade 50	(6.10.2.2-1)
$b_f \ge D/6$,	Too slender, D/4 better choice	(6.10.2.2-2)
$t_f \ge 1.1 t_w,$	Should be 1.5 to 2 x web thickness	(6.10.2.2-3)
and:		
$0.1 \le \frac{I_{yc}}{I_{yt}} \le 10$	Important limit, eliminates "T" like sections	(6.10.2.2-4)



3/8 in. Top Flange-1/2 in. Web

 $\frac{b_f}{2t_f} = \frac{16 \text{ in.}}{2 \times \frac{3}{8} \text{ in.}} = 21.3 > 12.0 \implies \text{NO GOOD}$





Flange Thickness Transition





Building a Girder





Raw Material

Longest Plate 80 feet Railcar





Mill Lead Times

A572 gr. 50 & A588 = 4 to 8 weeks HPS 70W = 4 to 10 weeks Rolled beams = 3 to 8 weeks

Material Not Stocked by Fabricator



Raw Material





First Steps

- Splice Flange and Web Plates
 - Full Penetration Weld
 - Nest Flange Plates if Possible
- Trim Mill Edges
- Rip Flange Plates to Width From Wide Plates (Cut Curve Small Radius)
- Cut Curve Webs for Desired Camber

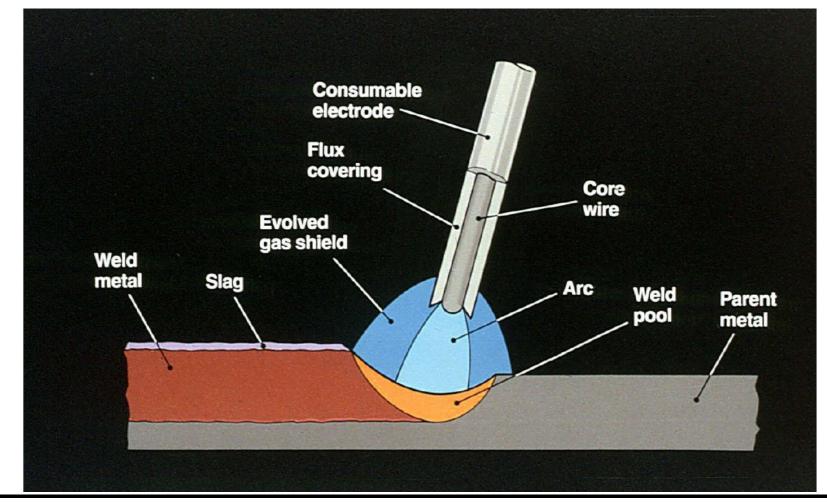


Welding

- Fusion Welding
 - Consumable Electrode and Base Metal Melted to Form Weld
 - Arc or Resistance Heating in the Flux
 Provides the Heat to Melt the Base Metal
 - Shielding Gas use to Protect the Molten Metal and Spray from Electrode Melting from the Atmosphere
 - Flux to Clean Molten Weld Pool and also used to Produce Shielding Gas in SMAW
- Base Metal Chemistry Must Be Controlled

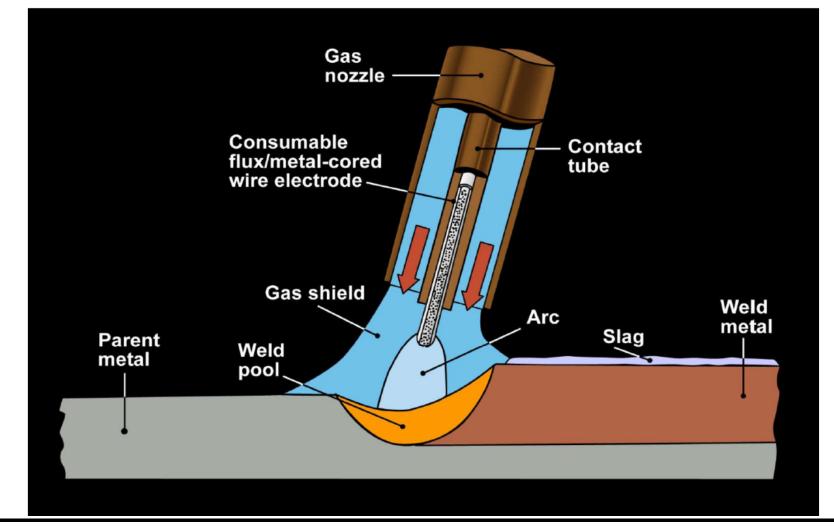


SMAW (Shielded Metal Arc Welding) Stick Welding



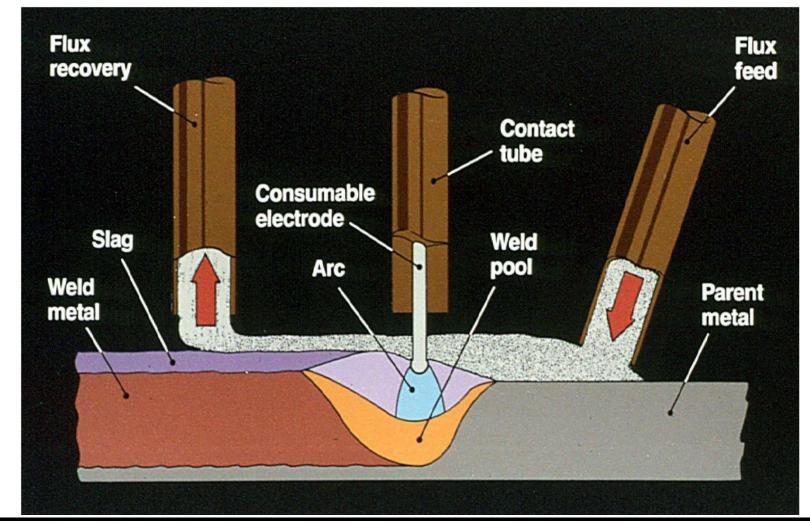


FCAW (Flux Cored Arc Welding)





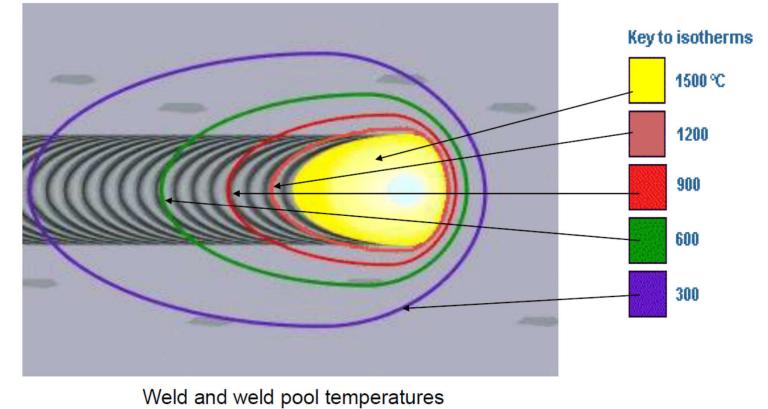
SAW (Submerged Arc Welding)



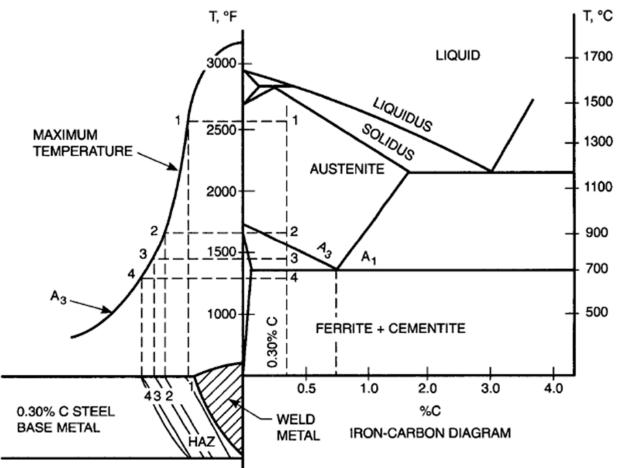


Cooling Weld by Conduction of Heat Into Plate

Thicker Plates Provide Larger Heat Sink Resulting in More Rapid Cooling



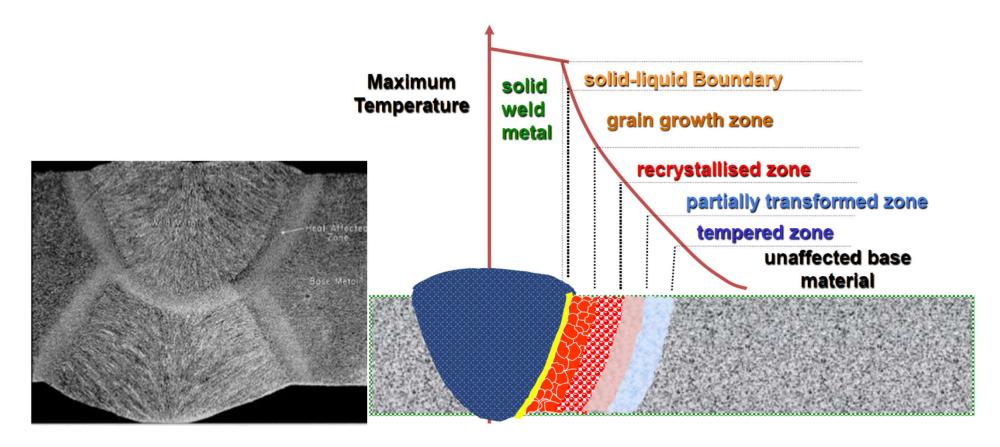
What Happens to Base Metal During Welding



Critical That Material Heated to Austenite Temperature is Cooled Slowly Enough to Not Form Martensite



Generation of Heat Affected Zone (HAZ)





Preheat and Interpass Temperatures AWS D1.5 Chap. 4

- Preheat- Temperature before welding
- Interpass-Temperature before starting next weld pass

Steel	To ³ ⁄ ₄ in. Incl.	³ ⁄₄ to 1- ½ in. Incl.	1- ½ to 2- ½ in. Incl.	Over 2- ¹ ⁄ ₂ in.
A709 Grade 36,50,50S,50W & HPS 50W	<u>></u> 50 ∘F	<u>></u> 70 ∘F	<u>></u> 150 ∘F	<u>></u> 225 ∘F
A709 Grade HPS 70W	50 to 450 °F	125 to 450 °F	175 to 450 °F	225 to 450 °F
A709 Grade HPS 100W	50 to 400 °F	125 to 400 °F	175 to 450 °F	225 to 450 °F

Higher Preheats Slow Cooling Rate



WPS

(Welding Procedure Specification) Qualification

- Purpose- Weld Metal Meets Mechanical Properties
 - Strength
 - Ductility
 - Notch Toughness Requirements
 - Done by Welding a Test Plate
- Generates a Procedure Qualification Record (PQR)
 - Documents Welding Variables
 - Documents Physical Test Results
- Exempt (Prequalified)
 - SMAW Welds (except E100 and E110)
 - Tack Welds Remelted by Subsequent SAW Welds
 - Welds of Ancillary Products



Heat Input

- Basis of Qualification Tests Limits
- Heat Input $\left(\frac{kJ}{in}\right) =$ Amperage x Voltage x 0.06

Travel Speed (in. per minute)

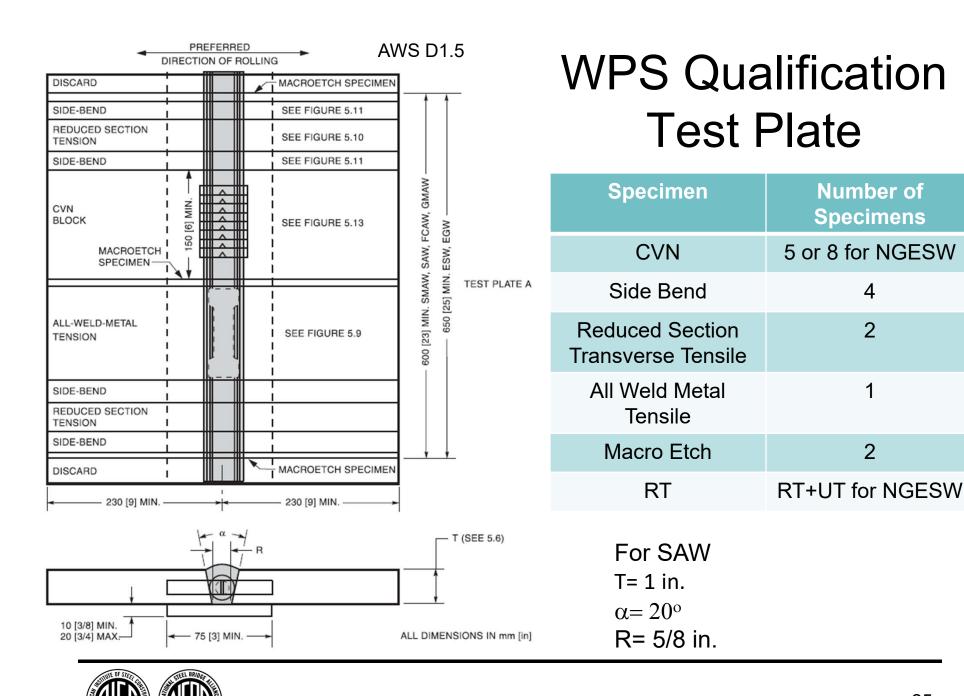
- Each pass with +/- 10% of overall average
 - Table 5.10 Gives Min. and Max. Amperage for each Process and Electrode Diameter



Qualification Options

- 5.12.1 Maximum Heat Input Qualification
 - Production Welds Heat Input <100% Qualification Test
 - Production Weld Heat Input> 60% Qualification Test
- 5.12.2 Maximum-Minimum Heat Input Qualification (Two Test Welds Required)
 - Production Heat Input Must be Between the Max. and Min. of Test Welds
- 5.12.4 Production Procedure Qualification
 - Multiple Pass SAW with Active Flux
 - Non Standard Joint Details
 - Matching Electrodes for HPS100W
- Most Procedures are Qualified Using 5.12.1





Test Requirements

Base Metal	Minimum Yield Strength (ksi)	Minimum Tensile Strength (ksi)	Minimum Elongation	CVN Zone I and II (ft-Ibs)	CVN Zone III (ft-Ibs)	Fracture Critical
Grade 36	45	60	22	20 @ 0ºF	20 @ -20°F	25 @ -20°F
Grade 50, 50S	50	65	22	20 @ 0ºF	20 @ -20ºF	25 @ -20°F
Grade 50W Grade HPS 50W	50	70	22	20 @ 0ºF	20 @ -20ºF	25 @ -20ºF
Grade HPS 70W	70	90	17	25 @ -10ºF	25 @ -20°F	30 @ -20ºF
Grade HPS 100W >2.5 in.	90	100	16	20 @ -40°F	Engr. Approval	35 @ -30ºF
Grade HPS 100W <u><</u> 2.5 in.	100	110	20	20 @-40ºF	Engr. Approval	35 @ -30ºF



Welding of Components

- Butt Welding of Flanges
 - SAW
 - NGESW
 - Nesting of Girder Flanges
- Welding Web to Flange
 - Plate Girders
 - Box/Tub Girders



SAW Weld Preparation Required to Get Access to Bottom of Weld





Prepared Plates Tacked Together Ready to Weld



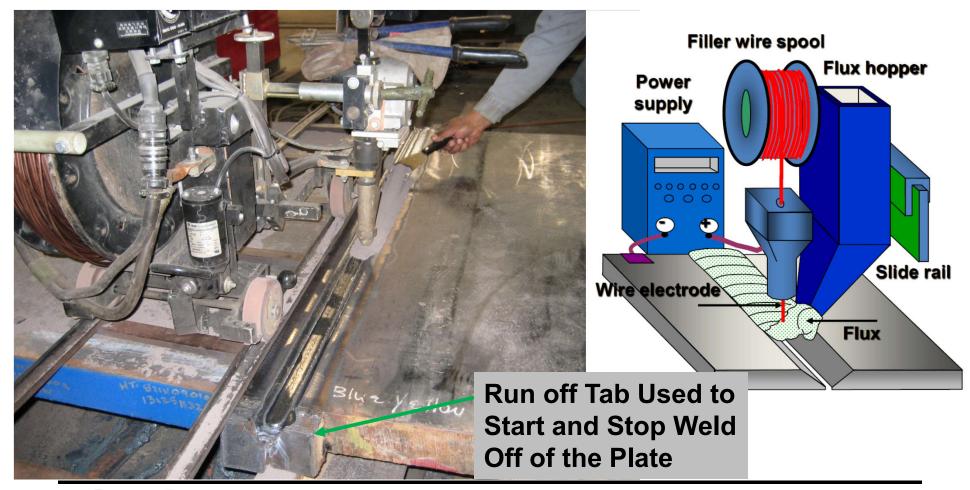


Flange Thickness Transition Note Weld in Thinner Plate at the End of The Transition





Submerged Arc Welding-SAW





Close Up of Arc Submerged in the Flux Multiple Pass Welds

Number of Passes Dependent Upon Plate Thickness



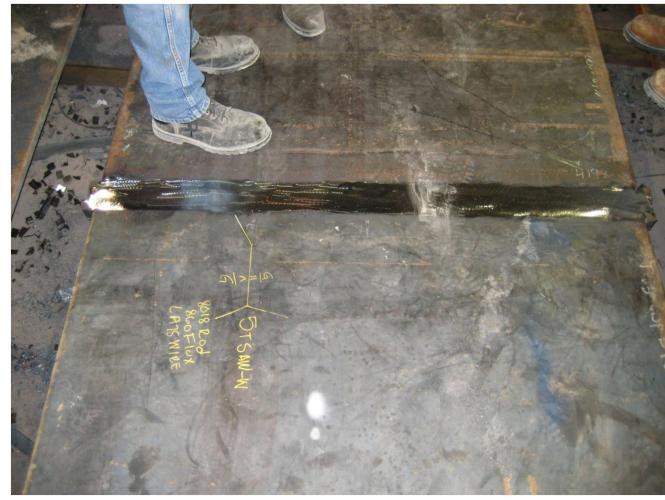


Back Gouge Weld Root and Clean By Grinding Weld Back Side





Finished Weld Ground Flush and Ready for Inspection by Radiography or Ultrasonics





Finished Flange Thickness Transition Butt Weld All Surfaces Ground Smooth





A New Way to Weld Narrow Gap Electroslag Welding





Narrow Gap Electroslag Welding NGEW

- Developed in an Extensive Research Study at the Oregon Graduate Institute by Wood and Turpin
- Based Upon Results of the Research, FHWA Lifted Moratorium March 2000
- Included in AWS D1.5 (2010)



Advantages of NSW for Flange Welds

- Single Pass Vertical Weld-No turning of plate and no back gouging
- Fast- Approximately 5 to 10 increase in productivity (2.5 to 1.5 in/minute, 3 foot long weld in about an hour)
- Completely Automated Equipment-Computer controlled wire and flux feed as well as voltage control

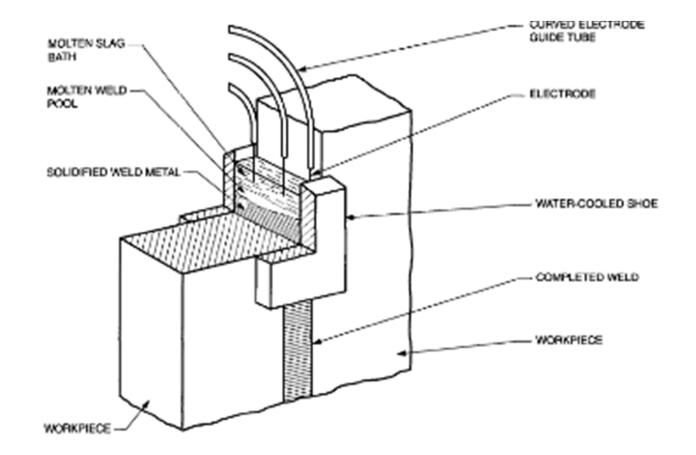


Characteristics

- Single Pass Vertical Up Weld
- Molten Weld Metal Contained by Water Cooled Copper Shoes
- Narrow Gap- 3/4 +/- 1/8 inch with square plate edge preparation
- Consumable Guide Tube to Guide
 Welding Wire
- Submerged Arc-Molten Flux Pool on Top of Weld Metal

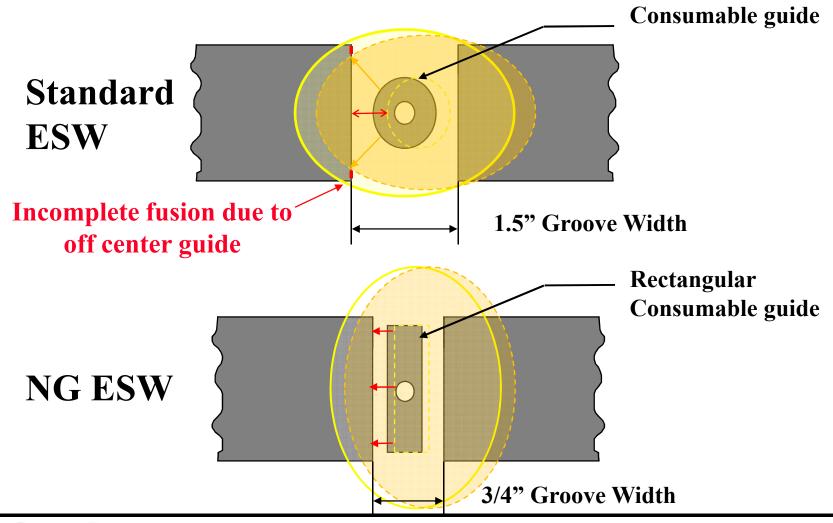


Schematic of ESW



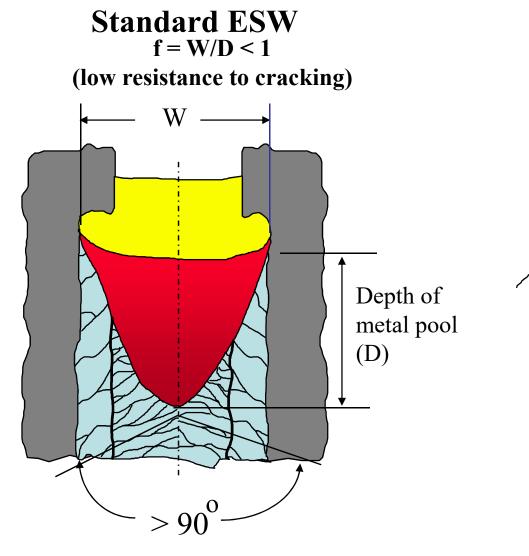


Narrow Gap Reduces Susceptibility to Incomplete Fusion

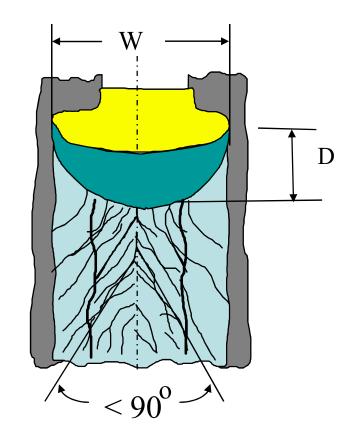




Enhanced Weld Pool Geometry



NG ESW f = W/D > 3 (high resistance to cracking)





Demonstration Weld to Show Flux Pool

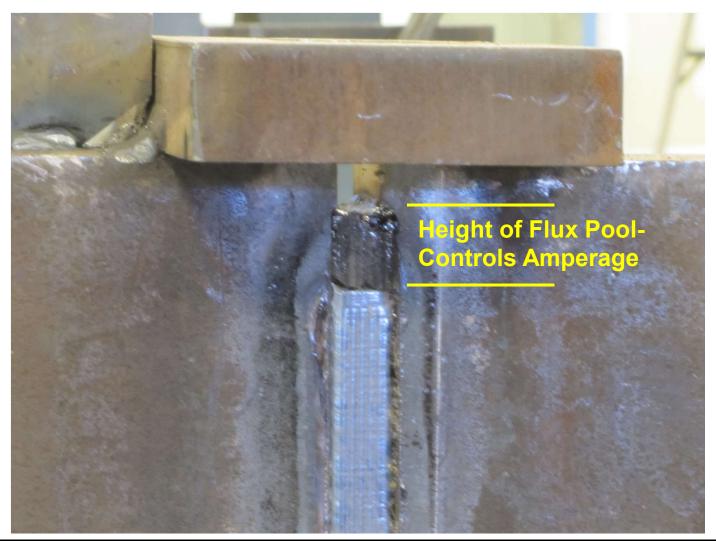




Plate Setup to Weld

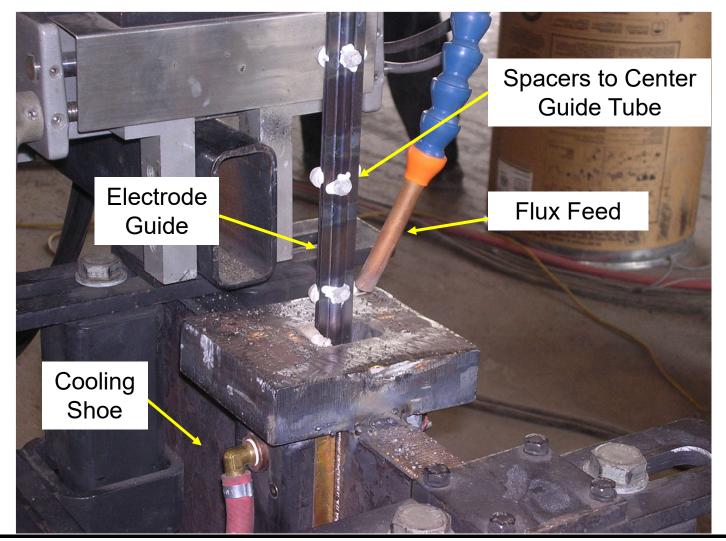


- Square Preparation
- Remove Mill Scale
 From Fusion Zone
- Sump at Bottom to Start Weld
- No Beveling or Turning of Plate
- Cast Weld Vertically
 in One Pass

Starting Sump



Final Preparation





Consumable Guide and Spacers





Plate Ready to Weld



• Water Cooled Copper Shoes to Contain Molten Weld Metal

> •Water Temperature and Flow Controlled to Produce Desired Cooling Rate

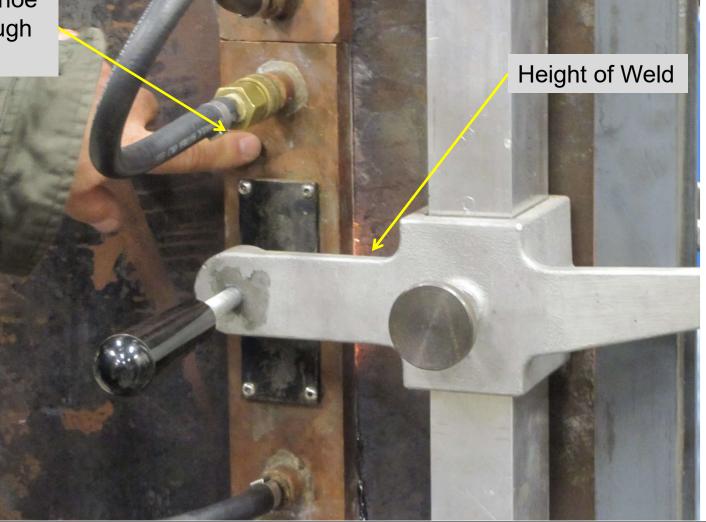
Automatic Process

Computer Controlled Wire FeedComputer Controlled Flux Addition



The Weld in Progress

Cooling Shoe Cool Enough to Touch





End of Weld



- Guide Consumed
- Note Molten Metal in Run Off Pad



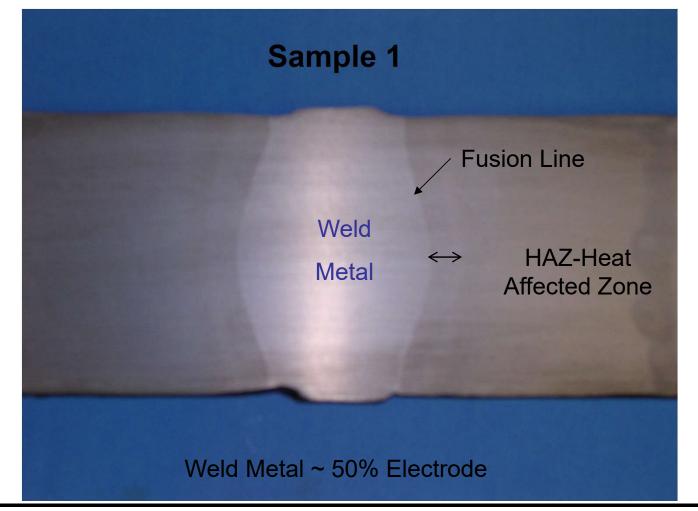
Completed Weld



Welding Time Approximately-10 to 20% of multiple pass weld *Minutes versus Hours*



Weld Cross Section





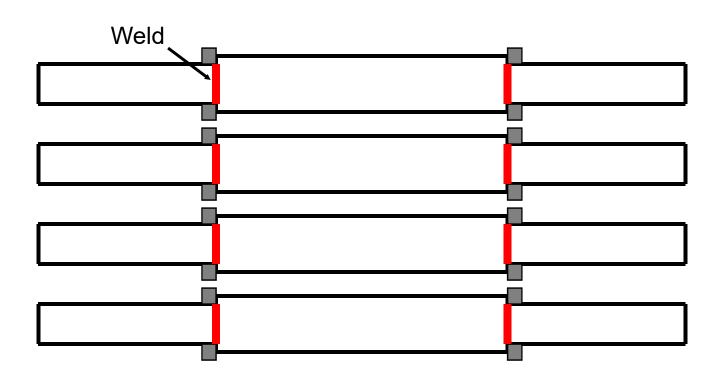
Efficient Flange Sizing

- Change Flange Width at Field Splice to Allow Welds to Be Slabbed
- Align Flange Thicknesses Transitions to Allow Slabbing
- Minimize the Number of Plate Thicknesses (plates come in 12 foot width and 80 foot lengths)
- Design it Like You are Going to Build it.



The Costly Method of Changing Flange Size by Changing Width

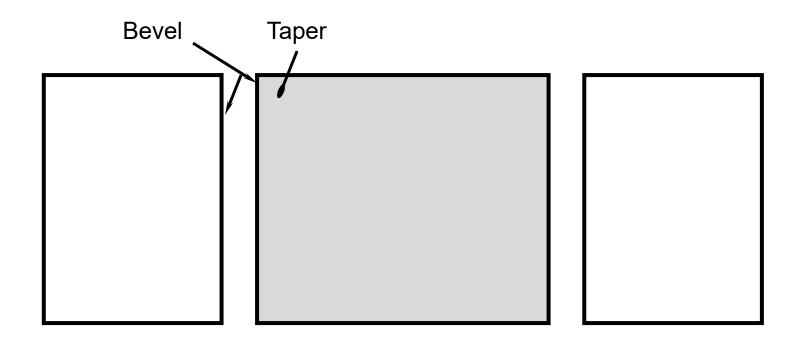
Weld and grind 8 splices





A Better Way- Change Flange Thickness

Bevel (4) and taper (2) plate edges

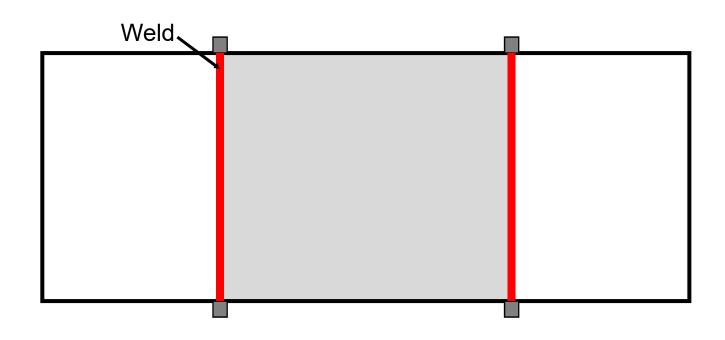


CHANGE THICKNESS



• Flange Sizing - change thickness

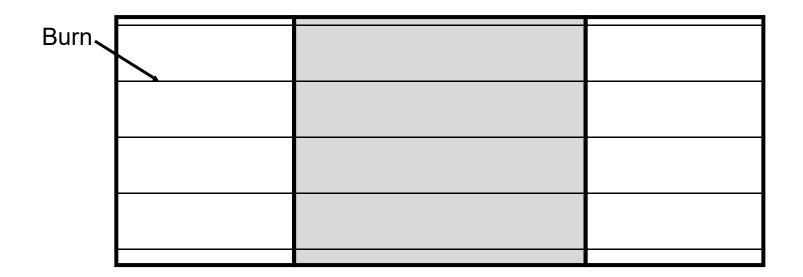
Weld and grind 2 splices





• Flange Sizing - change thickness

Burn 4 flanges from 1 assembly





• Flange Sizing - change thickness

4 flanges from 1 assembly



Good Practice

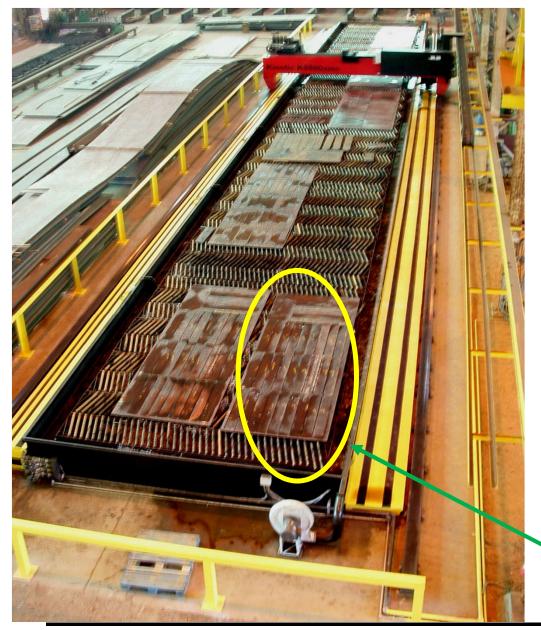
- Flange Sizing
 - Width transitions increase <u>labor</u> for flange assemblies up to 35%
 - If you must change flange width, do so at bolted field splice (do not clip corners of top flanges)
 - Allow fabricators to eliminate splices within a shipping piece by carrying thicker material through to next designed splice location



Plate Girder Flange Sizing

- Shop butt splices within a shipping piece when to change area?
 - No more than 2 shop splices
 - Minimum change; 1/8" (to 2 1/2" thick), 1/4"
 - Maximum change; thinner piece at least 1/2 of thicker...
 - <u>ONLY</u> when material cost saved > labor cost spent





CNC Cutting and Drilling Equipment

Equipment: 16.75 ft. x 165 ft. bed

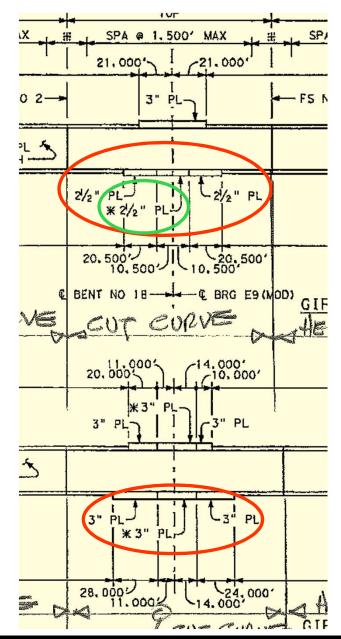
2-48 HP Drill Heads 12 tool Changer station

Plasma Automated Contour Bevel Cutting System

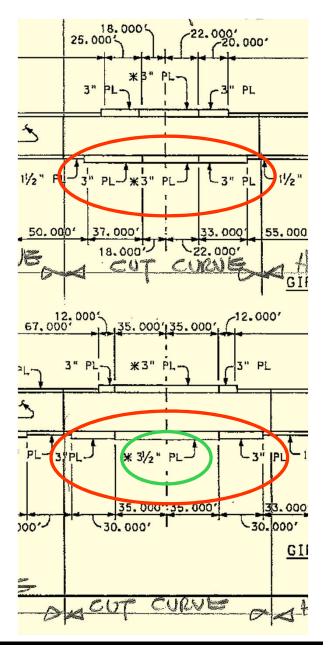
6-Oxy-Fuel Torch Stations

Flanges Stripped From Wider Plate



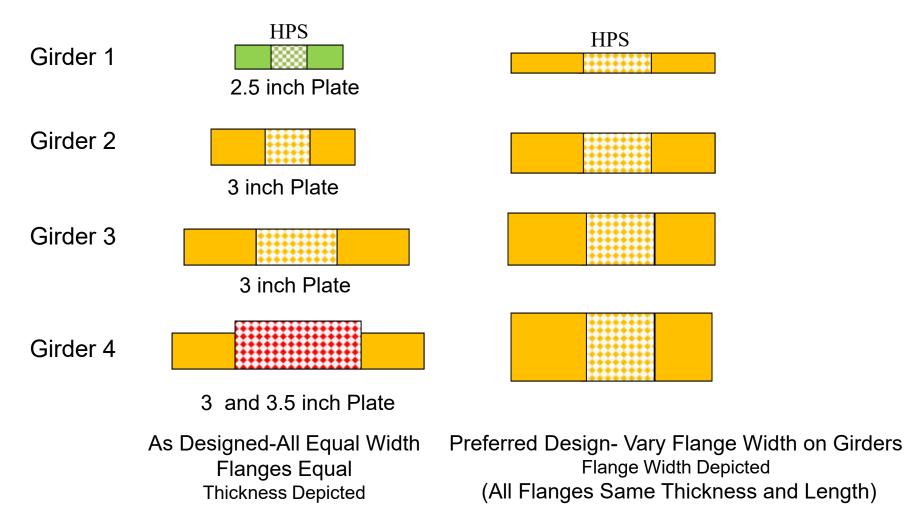








Bottom Flanges at Pier





Attaching the Web to the Flanges

- Plate Girders
- Box Girders



Assemble the Plates to Form Girder

Camber Cut Into Web

- Flanges Squeezed to Fit Cambered Web
- 2. Tack Welds

 Used as
 Temporary
 Connection
 Between The
 Web and Flange





SAW Welding the Flanges to the Web Tack Welds Consumed by SAW Weld



Weld Both Sides at Once

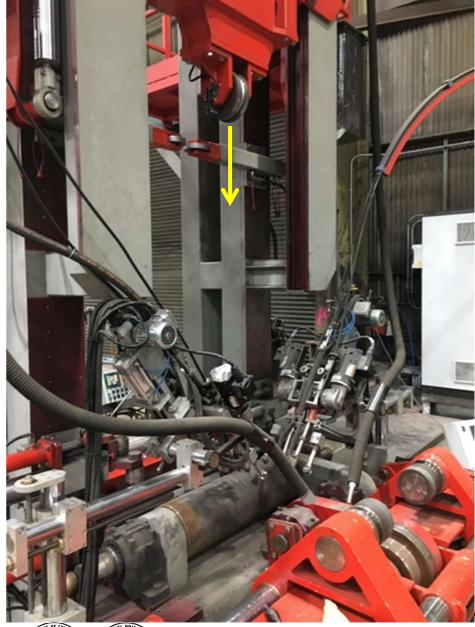
Welding Head and Preheat Torches

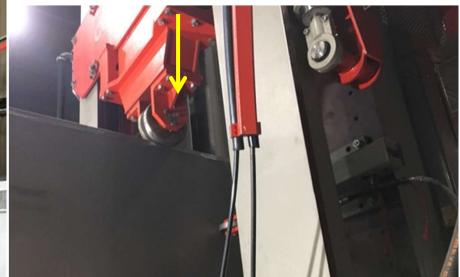


New Method of Assembly

- No Tack Welds
- Automated Welding Speed
- Preheat Built Into Fixture
- Welded T Assembly Flipped and Other Flange Welded







Clamping Force Applied by Roller at Top of Web



Web Centered on Flange Using Runoff Tab





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Girder Fed Into Welding Head by Rollers

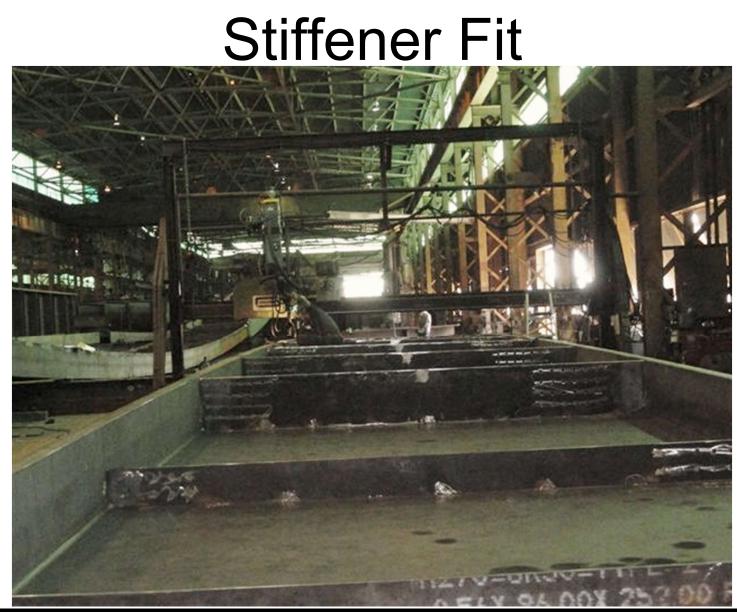




Frames to Steady Welded Section and Flip T Section









Stiffener Dart Welding SAW Both Sides Welded at the Same Time





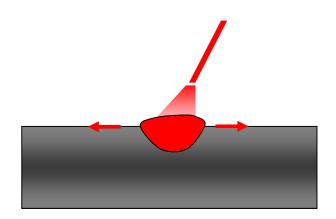
Tub (Box) Girders Hand Assembled



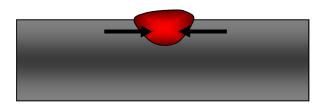
Flanges and Connection Plates Welded to Web Cross Frames Used to Control Box Geometry



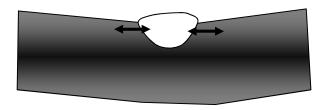
Residual Stress Due to Welding



Thermal expansion due to heat input from welding



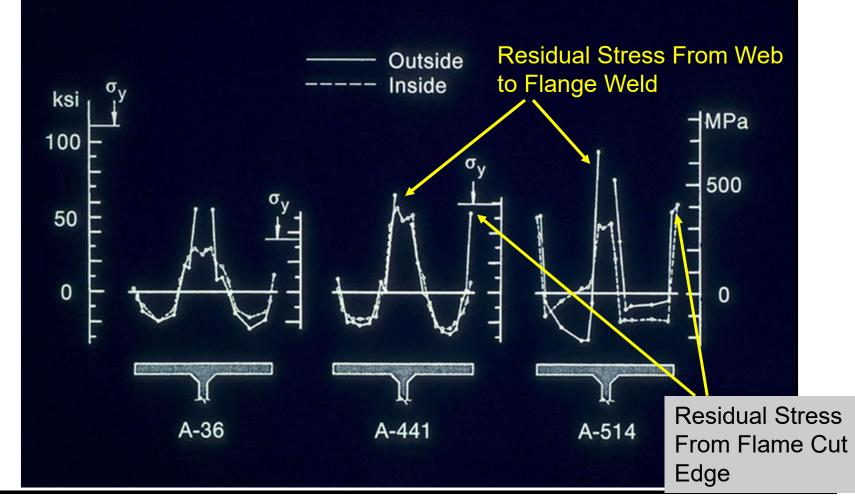
Shrinkage of beads due to cooling and solidification



Tensile residual stress in the vicinity of weld



Residual Flange Stresses in Welded Shape

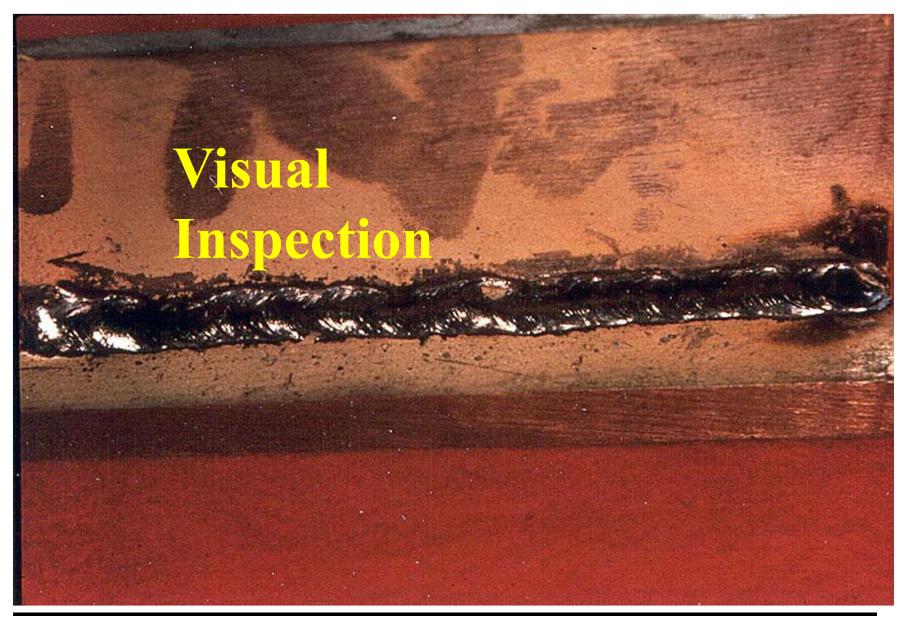




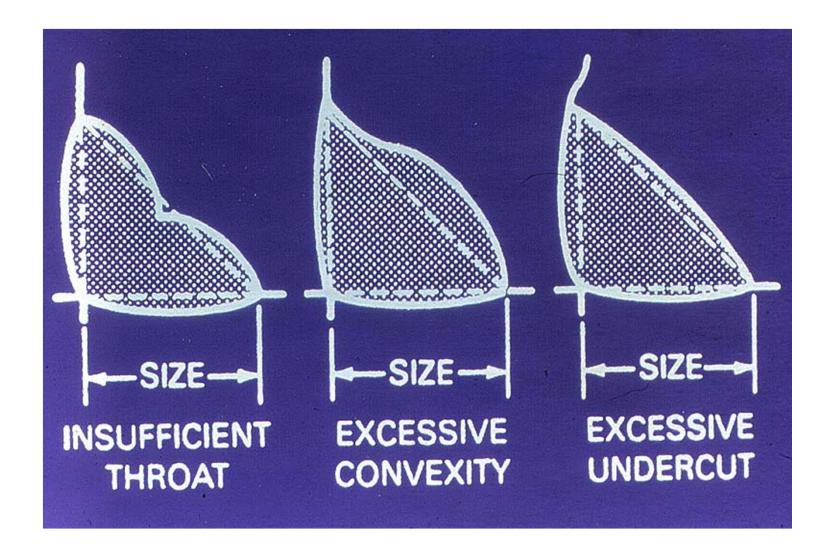
Weld Inspection

- Fillet Welds
 - Visual
 - Magnetic Particle
- Butt Welds
 - Ultrasonic
 - Radiography

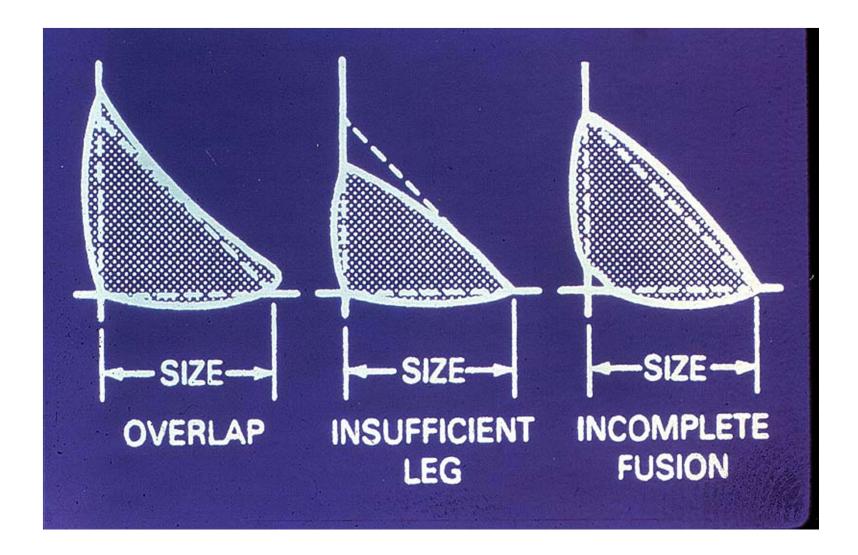










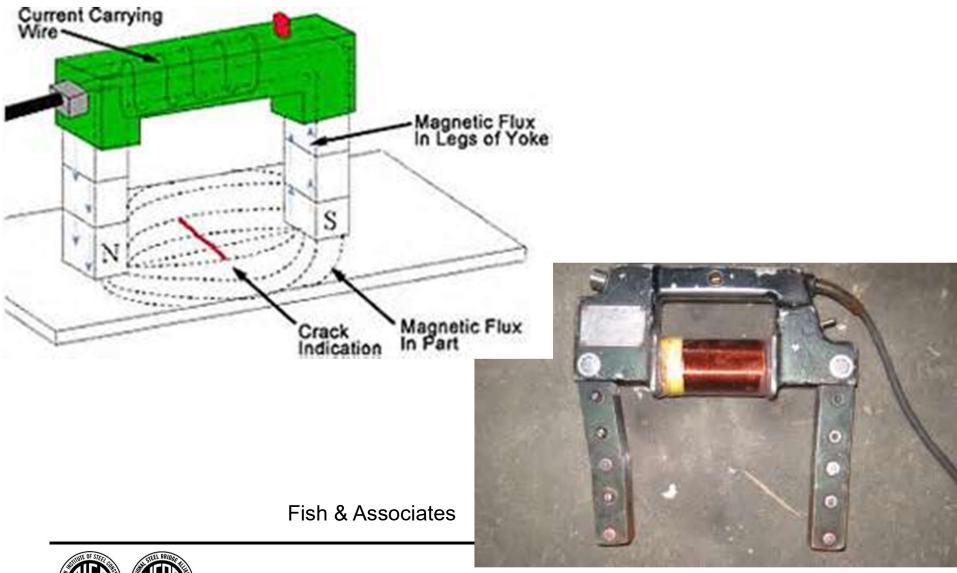




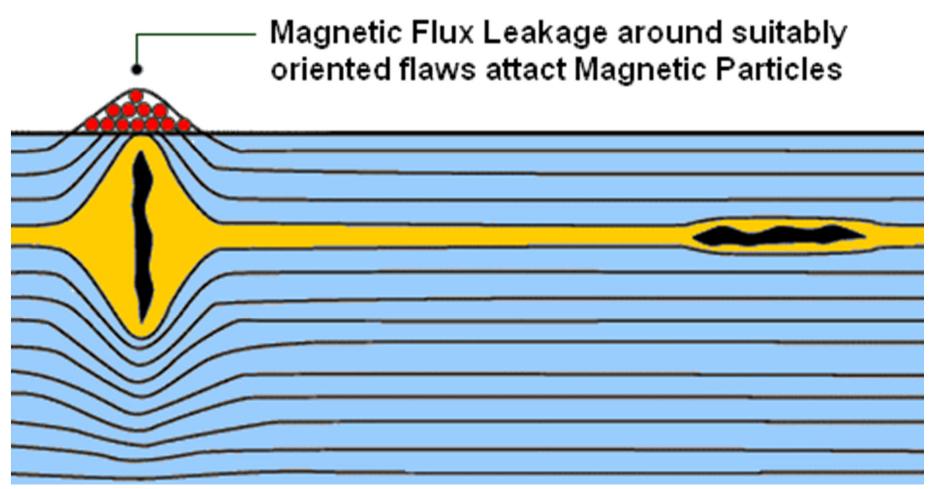
Magnetic Particle

- Inspection of Web to Flange Fillet Welds and Other Fillet Welds
- Surface or Near Surface Inspections



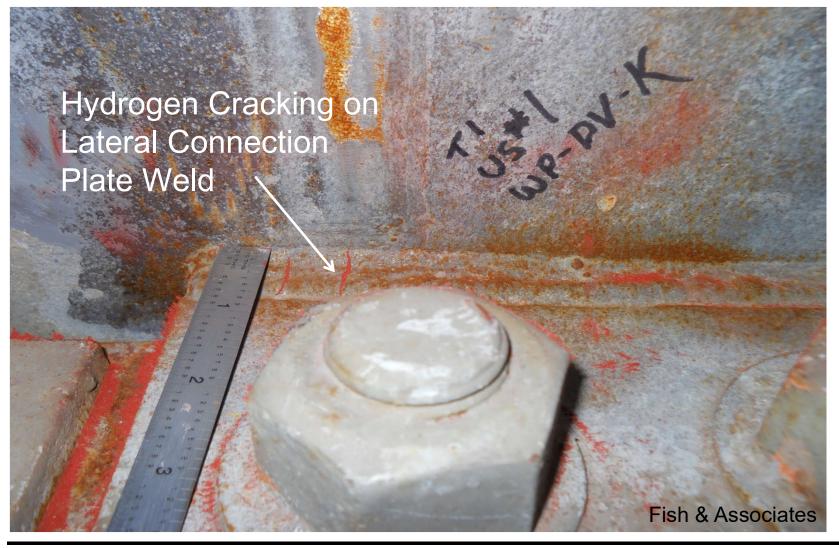




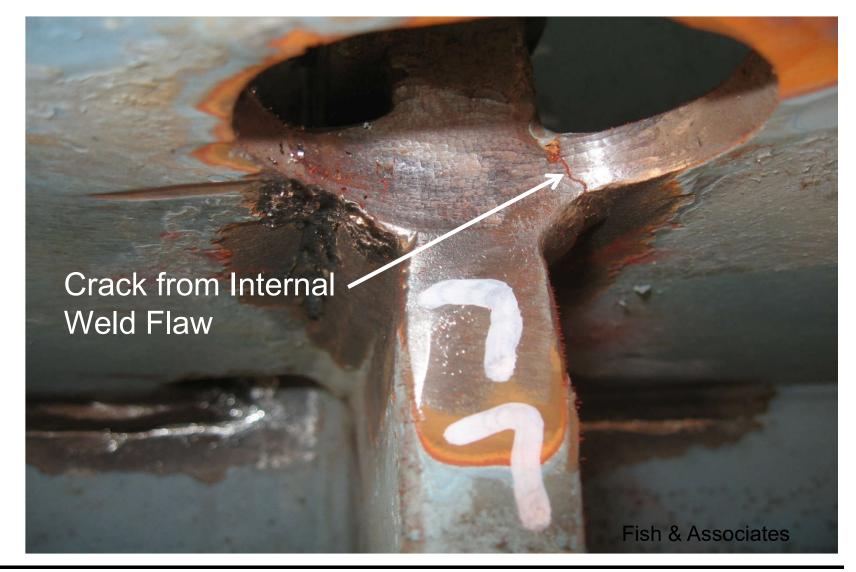


Fish & Associates









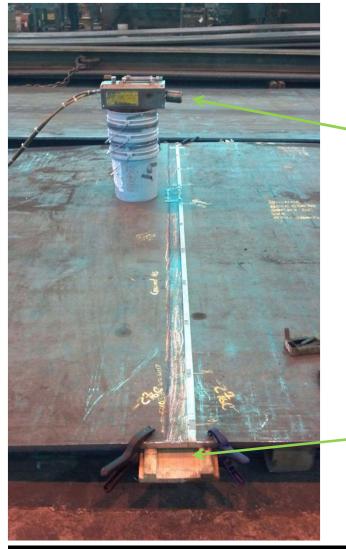


Radiography

- Gamma Ray (Nuclear) Source or X-Ray Source
- Internal Defects
- Very Good for Volumetric Defects
 - Slag
 - Porosity
- Provides a Visual Permanent Record on Film or Digital Record



Radiography



Gamma Ray Source

One Shot at a Timeabout 2 feet/per shot

Measures Density Along Ray Path

Film Holder



Radiation Hazard



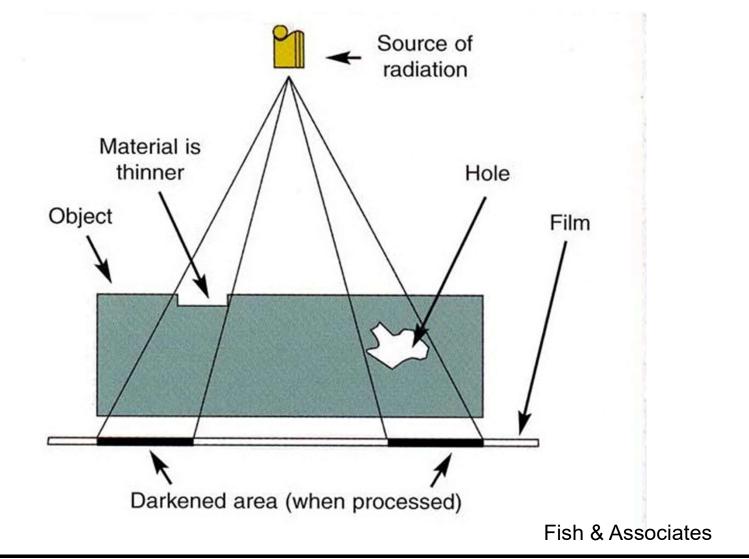
Weld

Inspect at Night Or Move Plate Out of Shop





Radiography (RT)

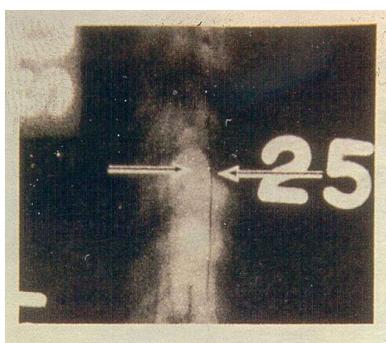


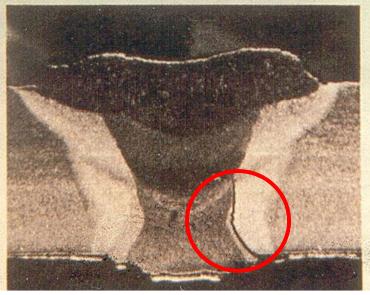


Approximate Thickness Limitations

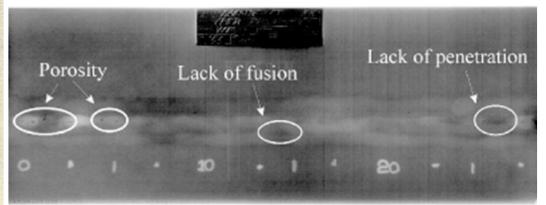
Radioisotope	Thickness, in.
Iridium-192	0.5-2.5
Cesium-137	0.5-3.5
Cobalt-60	>3









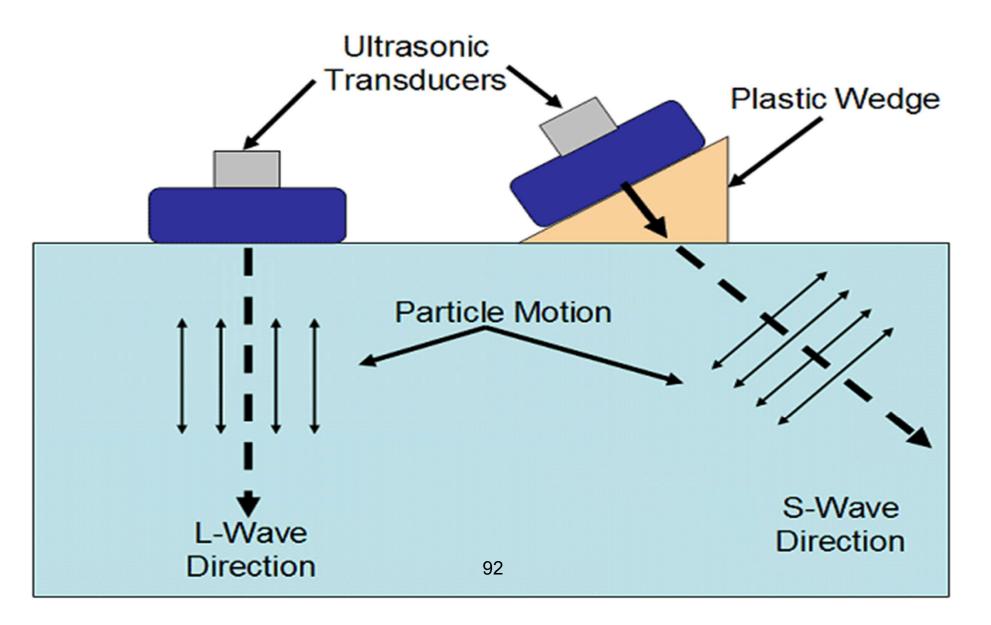


Ultrasonic Inspection

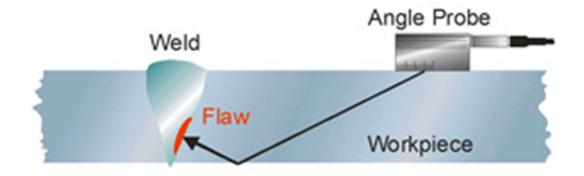
- Similar to Radar and Sonar
- Interrogate Weld Using High Frequency Waves (2-5 MHz)
- Sound Reflected Back to Transducer by Metal Air Interface (Defect)
- Portable and No Radiation Hazard

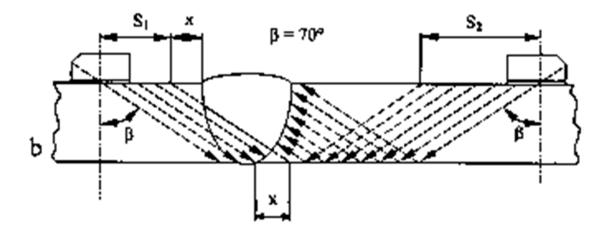


Conventional Ultrasonic Testing



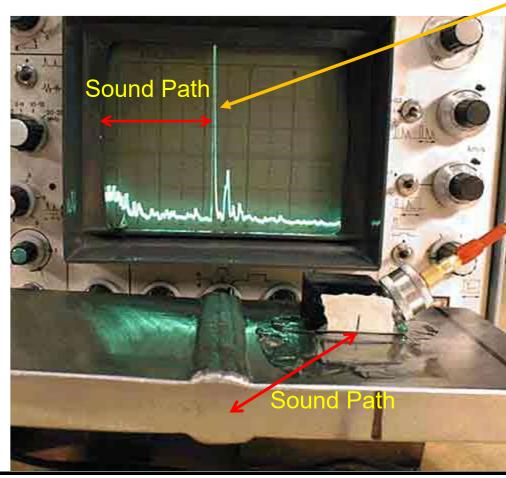
Ultrasonic Inspection







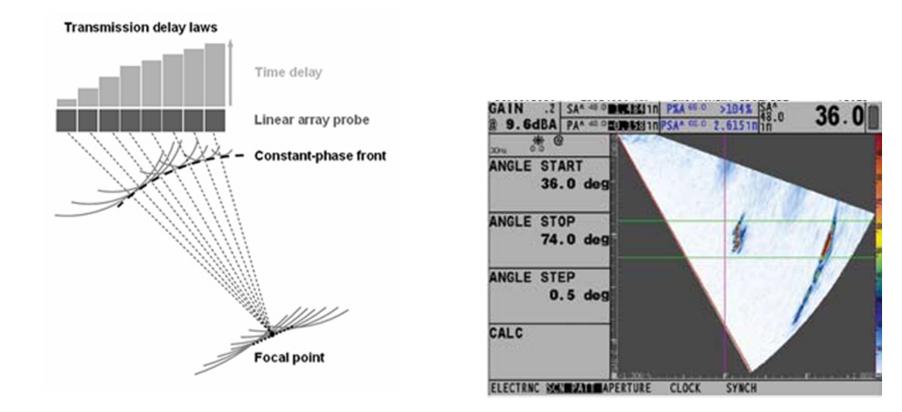
Angle Beam Testing of Weld



Amplitude of Reflected Sound Indication of Reflector Size



A New Technology Phased Array Ultrasonic Inspection



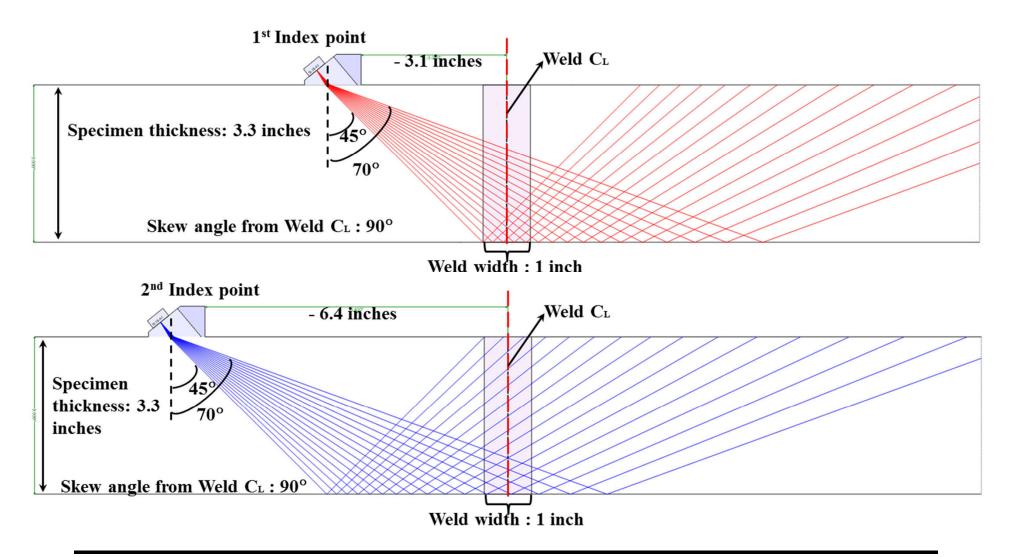


Transducer Contain Multiple Elements



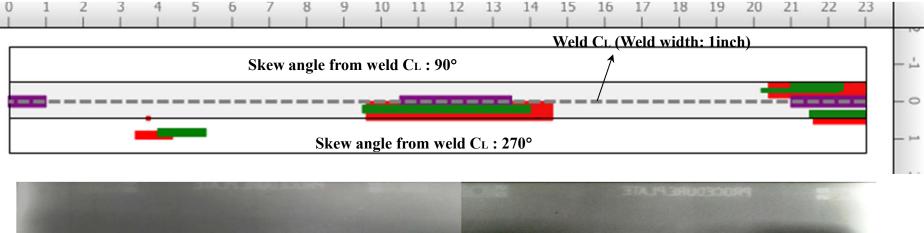


Typical Scan





UT Vs RADIOGRAPHY: SPECIMEN TP3 (TOP VIEW)

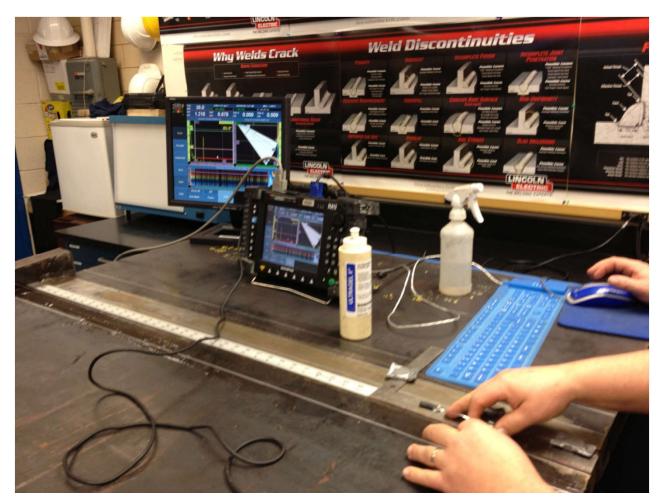




: PHASED ARRAY ULTRASONICS MEASUREMENTS AT TFHRC

- : SINGLE ELEMENT ULTRASONIC TESTING IN ACCORDANCE TO AWS D1.5 AT TFHRC
- : SINGLE ELEMENT ULTRASONIC TESTING IN ACCORDANCE TO AWS D1.5 BY FABRICATOR

Scanning Weld



Position Along Weld and Returned Signal Recorded Digitally



PAUT

- Digital Record of Inspection-not just an OK
- Less Operator Dependent but Requires Experienced User to Set Up Equipment
- Faster Than Conventional UT
- No Radiation Hazard
- Recognized in AWS D1.5



In Process Inspection





Heat Curved to Match Road Geometry





Girder Lay Down to Fit Field Splices



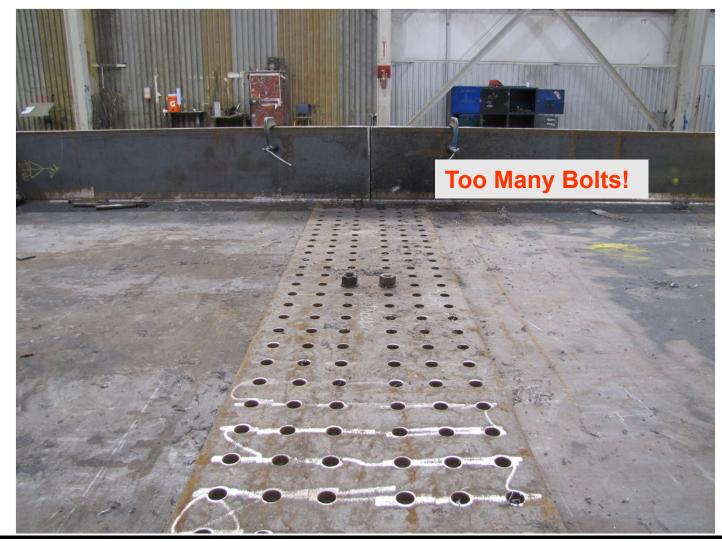


Flange Splice Splice Plate Used as Template





Web Splice





Match Drill Flanges and Webs Using Splice Plate for Template



- 1. Fabricate Splice Plates
- 2. Lay Down Girders
- 3. Clamp Plates to Girders
- 4. Match Drill



New Methods (Virtual Assembly) Eliminate Manual Drilling and Shop Assembly

Operations:

- 1. Cut and Drill Plates on Cutting Table
- 2. Assemble Girder-Weld Web to Flanges
- 3. Measure Girders to Determine Exact Hole Locations and Girder Geometry
- 4. Input Girder Geometry Into Computer
- 5. Assemble on Girders Virtually in Computer
- 6. Output Required Splice Plate Geometry to CNC Equipment

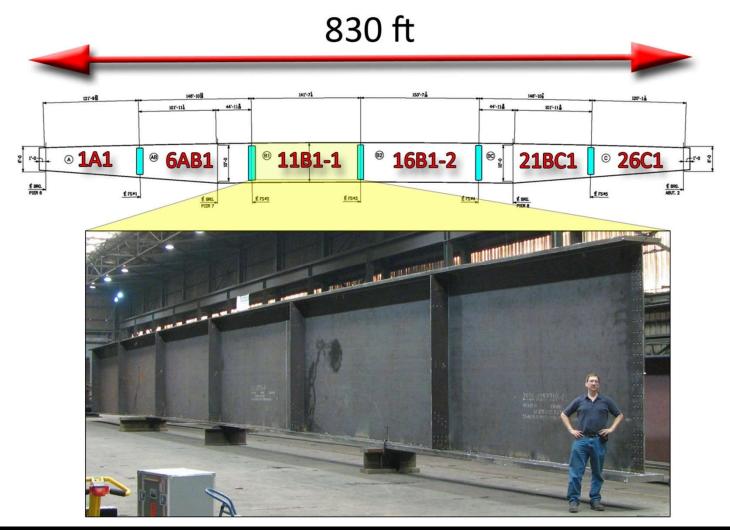


First Implementation

- Implemented in Virginia Sponsored Pooled Fund Study
 - Principal Investigator- Paul Fuchs (Fuchs Consulting, Inc.)
 - Tennessee DOT Bridge
 - Girder Fabrication by Hirschfeld Industries

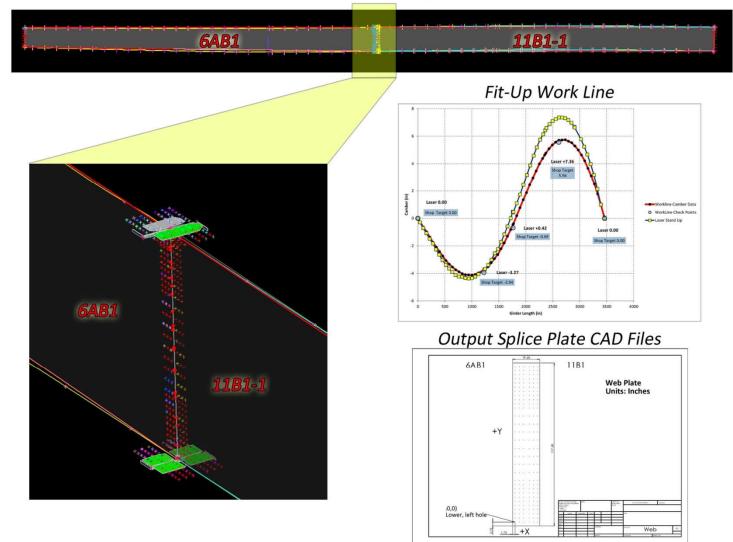


Tennessee DOT Bridge Job



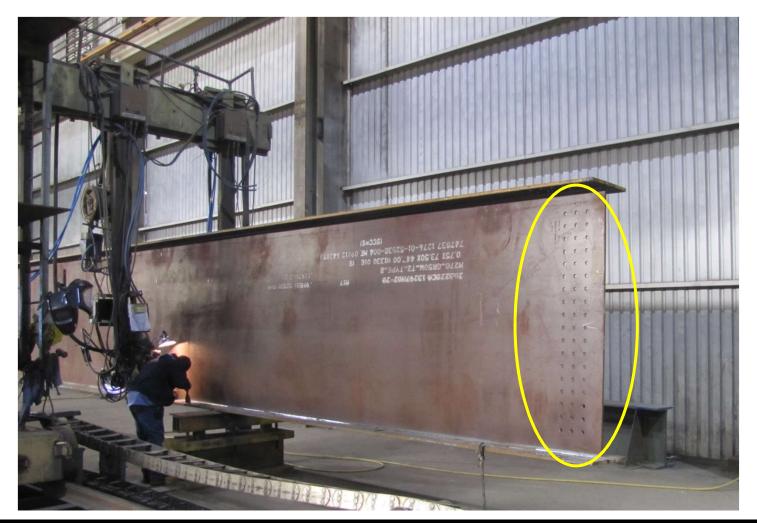


Virtual Assembly Software





Welding of Girder With Splice Holes





Predrilled Girders Trimmed and Adjusted for Correct Length and Camber





Hole Location Measurement Using Laser



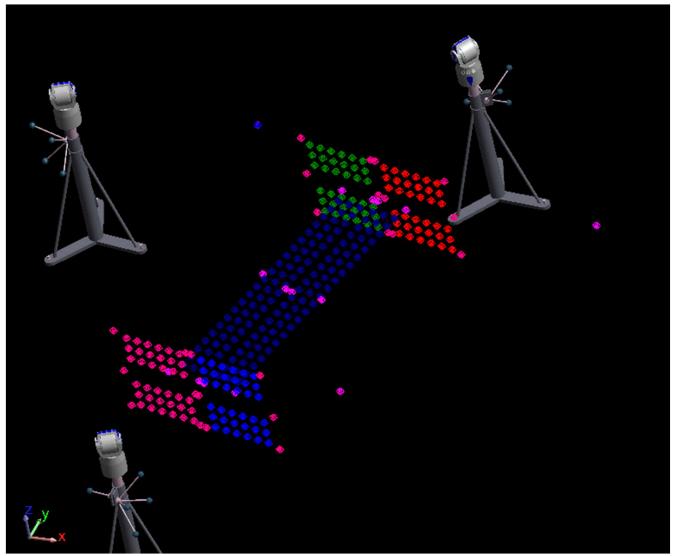


The Target-SMR Spherically Mounted Retroreflector



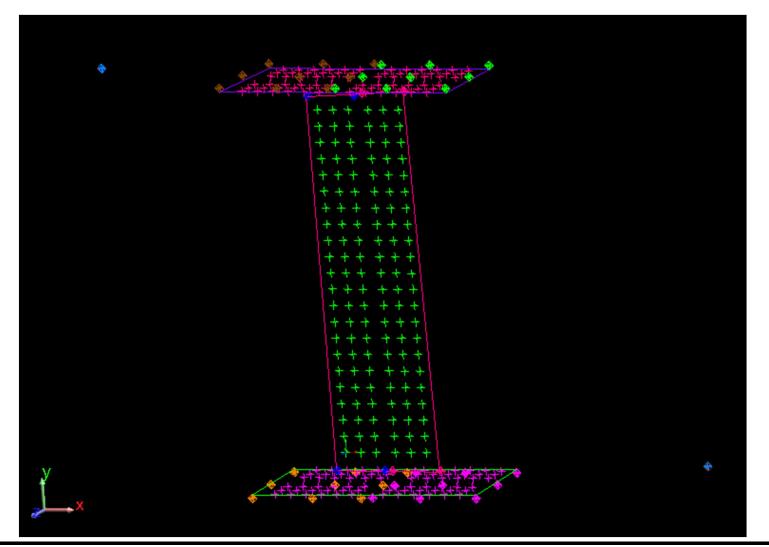


Scan Ends of Girders in Lay Down



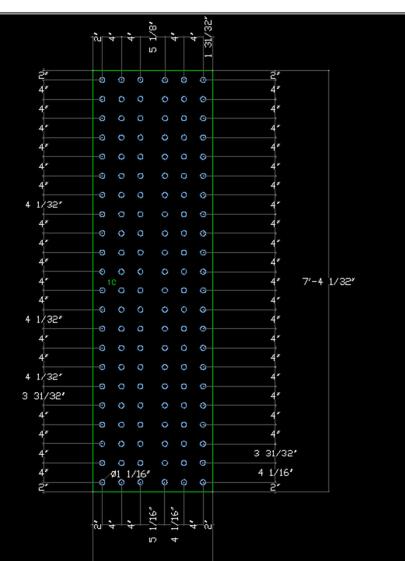


Development of Splice Plate Geometry





Splice Plate Detailed in Autocad



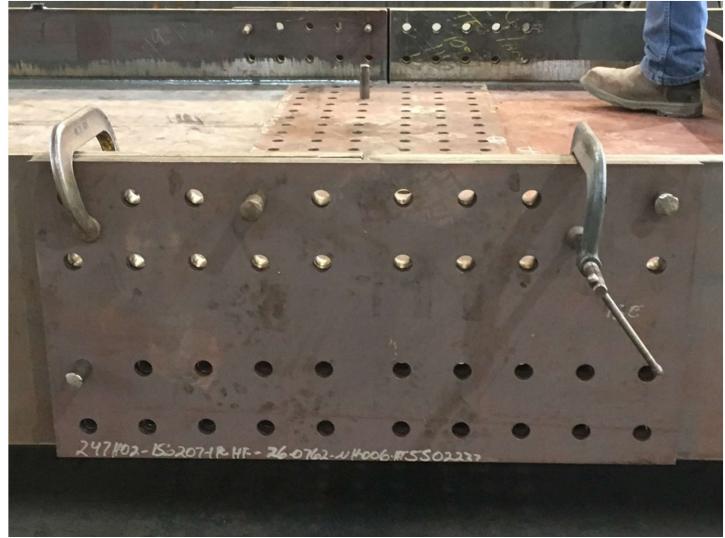


Check of Splice Plate Fitup





Flange Splice Fit





It Fits!





State of the Art

- Short Term:
 - Lay down two girders to determine splice geometry
 - Verify splice plate geometry by laser measurement
 - Verify fit up of stack up of splice plates and fillers on computer
- Long Term:
 - Full Virtual Assembly- Elimination of Lay Down of 2 Girders

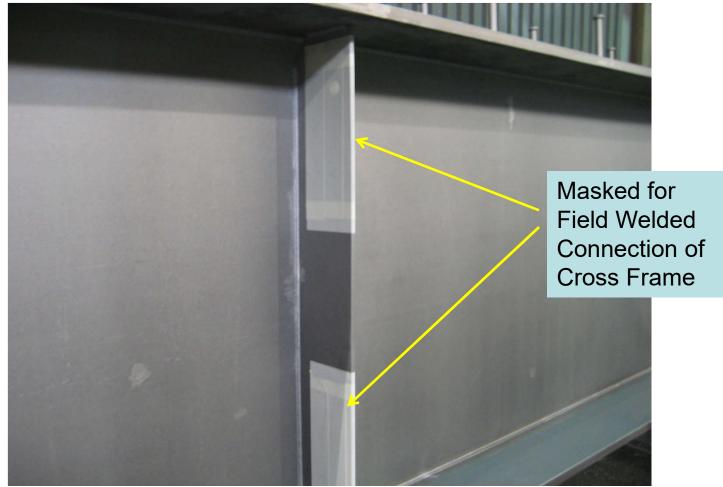


The Savings

- Reduced Material Handling-Drilling and Cutting in One Operation
- Speed- Hole Drilling About 10 times faster (3 seconds a hole)
- No Girder Lay Down Required (Girders can be fabricated in separate shops)



Girder Surface Prepared by Blasting Before Painting





Blasted Curved Girder





Painting Often 3 Coats







Final Inspection



Final inspection is performed first by in-house QC department and lastly by the owner's quality representative



Over Road Shipping





Too Tall-Ship with Web Flat



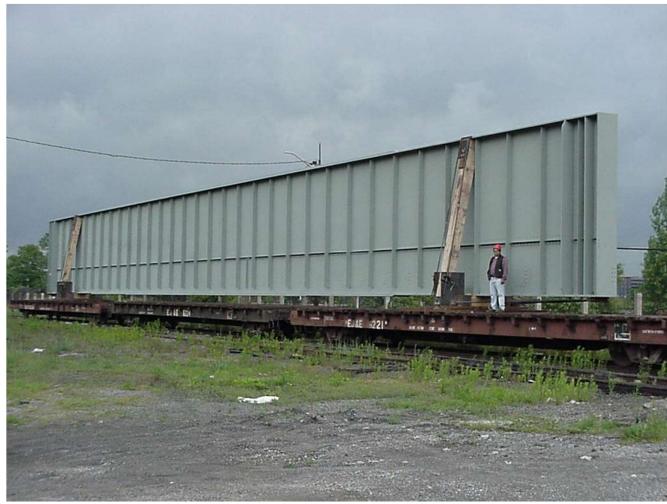


Super Loads Require Escorts and Special Permits





Too Long and Too Tall-Railroad as Last Resort





Tappan Zee Girders Loaded On Barge For Shipment From North Carolina to Hudson River Assembly Site





Optimal Fabrication Capacities Transportation Limits

Standard Up to 120" Girders depths with parallel Flanges Up to 144" Haunched Girders Conditional Up to 168" with State permission for

Girder lay down during shipment



Shipping Permits

Annual Permit

12' wide and 75' long or less

Travel only allowed on Non Posted Roads and Bridges – Specified Routes if over 80 kip

Single trip Permit

15' Wide, 14' Tall, Max. Length120' Over 14' tall loads require 2 more days review time Gross weight Limits

5 Ăxle 112,000 Lbs 6 Axle 120,000 Lbs 7 Axle 132,000 Lbs

Superload Permit

Over 120' in length

10 day Minimum Review Time

Gross weight > 132 kip requires 3 additional days for Bridge review



Summary

- Welding and Weld Inspection
 - D1.5 Controls
 - PQR Demonstrate Ability of Fabricator to Make the Weld
 - WPS is the Procedure Based Upon the PQR
 - Thicker Higher Strength Plates Require Higher Preheats and Greater Welding Skill
 - SAW is the Most Common Welding Process
 - NGESW Gaining Popularity
- Weld Inspection
 - RT is Slow and Dangerous, Film Record
 - UT Portable and Fast, no Record
 - PAUT Ease of UT with Digital Record



Summary

- Residual Stresses are Unavoidable and Not Calculated
- Virtual Assembly Field Spices on the Computer
 - Proven Technology Used in Other Industries
 - Provides a Digital Record of Fitup
- Design it Like You are Going to Build It
 - Avoid Short Lengths of Unique Plates
 - Space Welded Splice to Allow Slabbing of Welds
 - Size Field Pieces to Shipping Lengths
 - Ask the Fabricator About Any Questions



Good Design of Simple Bridge





A New Day Another Bridge





Questions?

